

RoadCem Bound Soil Piling Platforms Sustainable, Safe and Sensible.



PowerCem Technologies – Who are we?

PowerCem Technologies BV, established in 1996

- UK Office:- Founded 2011 in Derby
- Based in Moerdijk, The Netherlands
- Specialisation: Improving cement-bound materials
- Products used worldwide





PowerCem Global Partner Network

POWERCEM WORLDWIDE



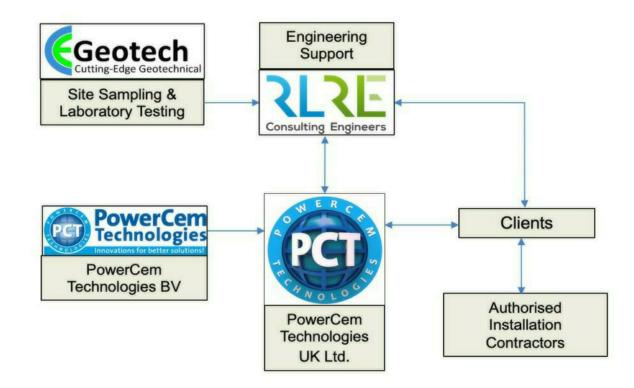
Globally RoadCem has stabilised over 11,500,000m² of soils







PowerCem Technologies in the UK



PowerCem Technologies in the UK



Rodgers Leask Consulting Engineers

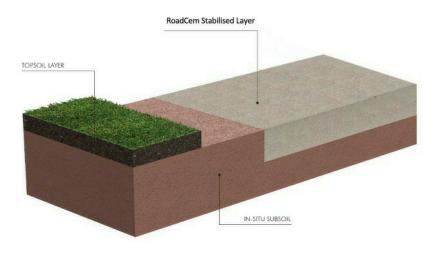
- Engineering partners to PowerCem UK
- Independent third-party organisation with offices in Derby, Birmingham, Bristol, Liverpool and Nottingham
- Providing:-
 - Site sampling and lab testing co-ordination
 - Design analysis, calculations and specifications
 - Optimised mix designs to meet client requirements
 - Technical liaison for client, contractor and consultants
 - Design Performance Warranties & Piling mat certification for all rig types





RoadCem Soil STABILISATION: Single Layer Piling Platforms

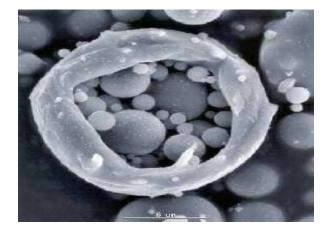
- Controlled mixing of a cementitious binder and RoadCem additive directly into soils at varying degrees of moisture content
- Improves the compressive strength and flexural stiffness and most importantly creates a piling mats with high visco-elastic properties which absorbs vibration
- Produces robust PERMANENT changes in soil material properties such as STRENGTH, DURABILITY and DUCTILITY which prevents cracking & breakaway
- Waterproof layer no softening of stabilised layer in saturated soils or flood events
- High resistance to expansive secondary sulphate reaction
- Can be used with over-wet soils or those with higher organic contents >5%
- Lower residual pH levels after curing compared to pure cement binders



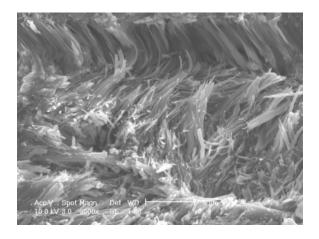


- PowerCem products are an inert blend of synthetic Zeolites, alkali earth metals and other natural minerals
- They act as a catalyst to improve the end performance characteristics of the cementitious products in question
- This is often referred to as 'Nanotechnology'

Traditional Cement



Cement glues the aggregate particles together forming a 'brittle bond' Cement with RoadCem additive:



Cement with RoadCem forms needle like elements , **interlocking** the aggregate particles in a 'flexible matrix'



Based on a large number of piling mat projects around the World and at the request for design information, we have made a general table for the thickness of this type of construction for all different UK in-situ soil types.

Due to the fact that the type of vehicles during the "lifetime" of this construction is on all the sites practically the same:

- pilling drilling machines
- trucks, that are delivering the piles

Based on the Bearing Capacity an estimation of the type of soil is made and a mix design is estimated and the mechanical properties of the stabilisation (1).

These mix designs are indicative, and might need to change if local circumstances are requiring this (large amounts of organic material in soil).

For the calculation of the bending moments, strains under the tires of the trucks (2) the multi-layer elastic methodology is used.

With the computer program BISAR the stresses and strains are determined.

For the calculations for the minimum thickness of the pilling drilling machines (3), the Hetenyi Method was used. With this method the bending moment, and the shear strength can be accurately determined under the specific continuous tracks of the pilling drilling machines.



1. Mix Designs and mechanical properties of the stabilised material.

| Sub grade | Modulus of subgrade reaction | Soil type | RoadCem | Cement | Stiffness | Breaking strain | Flexural strength | Shear strength |
|-----------------|------------------------------------|--------------|----------------------|----------------------|-------------|--------------------|-------------------|-------------------|
| [Edyn: MPa] | [N/mm ³] | | [kg/m ³] | [kg/m ³] | [Edyn: MPa] | [µm/m] | | |
| <mark>20</mark> | 0,020 | Clay | 2,4 | 240 | 2500 | 240 | 0,75 | 0,50 |
| <mark>30</mark> | 0,025 | Clay | 2,2 | 220 | 3000 | 230 | 0,90 | 0,60 |
| <mark>40</mark> | 0,030 | Clay | 2,2 | 220 | 3500 | 210 | 1,05 | 0,70 |
| 50 | 0,035 | Clay | 2,0 | 200 | 4000 | 190 | 1,20 | 0,80 |
| <mark>60</mark> | 0,040 | Sandy clay | 1,8 | 180 | 4500 | 170 | 1,35 | 0,90 |
| 70 | 0,045 | Sandy clay | 1,8 | 180 | 4500 | 170 | 1,35 | 0,90 |
| <mark>80</mark> | 0,050 | Sandy clay | 1,8 | 180 | 4500 | 170 | 1,35 | 0,90 |
| 90 | 0,055 | Sand | 1,6 | 160 | 5000 | 150 | 1,50 | 1,00 |
| 100 | 0,060 | Sand | 1,6 | 160 | 5000 | 150 | 1,50 | 1,00 |
| 110 | 0,065 | Sand | 1,6 | 160 | 5000 | 150 | 1,50 | 1,00 |
| 120 | 0,080 | Sandy gravel | 1,4 | 140 | 5500 | 140 | 1,65 | 1,10 |
| 130 | 0,085 | Sandy gravel | 1,4 | 140 | 5500 | 140 | 1,65 | 1,10 |
| 140 | 0,090 | Sandy gravel | 1,4 | 140 | 5500 | 140 | 1,65 | 1,10 |
| 150 | 0,095 | Sandy gravel | 1,4 | 140 | 5500 | 140 | 1,65 | 1,10 |



2. Calculation of the stresses and strains for the heavy truck that are delivering the piles.

For the calculation we assumed a standard axle load of 100 kN, with 4 wheels per axle.

| | | PROPER | FIES | | | DESIGN | | | |
|--------------------|--|--------------|--------------------|------------|---------------------------------------|------------------------------|------------------|------------------|--|
| Sub grade | Modulus of subgrade reaction [N/mm ³] | Soil type | RoadCem [kg/m²] | Cement | Stiffness [E _{dyn} : MPa] | Minimum Thickness [cm] | Strain [µm/m] | Safety factor | |
| 20 | 0,020 | Clay | 2,4 | 240 | 2500 | 30 | 202 | 1,19 | |
| 30 | 0,025 | Clay | 2,2 | 240 220 | 3000 | <mark>25</mark> | 214 | 1,07 | |
| 40 | 0,030 | Clay | 2,2 | 220 | 3500 | <mark>25</mark> | 179 | 1,17 💈 | |
| 3 <mark>50</mark> | 0,035 | Clay | 2 | 200 | 4000 | <mark>25</mark> | 148 | 1,30 💈 | |
| 80 | 0,040 | Sandy clay | 1,8 | 180 | 4500 | <mark>25</mark> | 134 | 1,27 💈 | |
| 2 <mark>70</mark> | 0,045 | Sandy clay | 1,8 | 180 | 4500 | <mark>25</mark> | 130 | 1,31 💈 | |
| 80 | 0,050 | Sandy clay | 1,8 | 180 | 4500 | <mark>25</mark> | 128 | 1,35 💈 | |
| 2 <mark>90</mark> | 0,055 | Sand | 1,6 | 160 | 5000 | <mark>25</mark> | 113 | 1,33 🖕 | |
| 100 | 0,060 | Sand | 1,6 | 160 | 5000 | <mark>25</mark> | 110 | 1,36 💈 | |
| 2 <mark>110</mark> | 0,065 | Sand | 1,6 | 160 | 5000 | <mark>20</mark> | 146 | 1,03 💈 | |
| 120 | 0,080 | Sandy gravel | 1,4 | 140 | 5500 | <mark>20</mark> | 133 | 1,05 🕺 | |
| 2 <mark>130</mark> | 0,085 | Sandy gravel | 1,4 | 140 | 5500 | <mark>20</mark> | 130 | 1,08 💈 | |
| 2 <mark>140</mark> | 0,090 | Sandy gravel | 1,4 | 140 | 5500 | <mark>20</mark> | 127 | 1,10 💈 | |
| 2 <mark>150</mark> | 0,095 | Sandy gravel | 1,4 | 140 | 5500 | <mark>20</mark> | 125 | 1,12 💈 | |



3. Calculation of the stresses and strains for the pilling drilling machine.

For the drilling machine the following assumptions are made:

Type of drilling machine:

Woltman THW 4017

Weight 40 ton

Tracks 900 x 4850mm

| | | PROPE | ERTIES | | | DESIGN | | | | |
|-------------------------------|---|--------------|--------------------|--------|-----------------------------|-------------------|-------------------------------|------------------------------|-----------------------|--------------------------|
| Sub grade [Eao: MPa] | Modulus of subgrade reaction [N/mor ³] | Soil type | RoadCem [kg/m³] | Cement | Stiffness [Edvn: MPa] | Thickness [cm] | Flexural s Stress [MPa] | trength. safety factor | sł Stress [MPa] | near safety factor |
| 20 | 0,020 | Clay | 2,4 | 240 | 2500 | <mark>55</mark> | 0,69 | 1,09 | 0,10 | 5,00 |
| <mark>30</mark> | 0,025 | Clay | 2,2 | 220 | 3000 | <mark>45</mark> | 0,92 | 0,98 | 0,12 | 5,00 |
| <mark>40</mark> | 0,030 | Clay | 2,2 | 220 | 3500 | <mark>35</mark> | 0,99 | 1,06 | 0,15 | 4,67 |
| <mark>50</mark> | 0,035 | Clay | 2,0 | 200 | 4000 | <mark>30</mark> | 1,19 | 1,01 | 0,18 | 4,44 |
| <mark>60</mark> | 0,040 | Sandy clay | 1,8 | 180 | 4500 | <mark>30</mark> | 1,18 | 1,14 | 0,18 | 5,00 |
| <mark>70</mark> | 0,045 | Sandy clay | 1,8 | 180 | 4500 | <mark>25</mark> | 1,31 | 1,03 | 0,21 | 4,29 |
| 80 | 0,050 | Sandy clay | 1,8 | 180 | 4500 | <mark>25</mark> | 1,25 | 1,08 | 0,21 | 4,29 |
| <mark>90</mark> | 0,055 | Sand | 1,6 | 160 | 5000 | <mark>20</mark> | 1,48 | 1,01 | 0,27 | 3,70 |
| <mark>100</mark> | 0,060 | Sand | 1,6 | 160 | 5000 | <mark>20</mark> | 1,42 | 1,06 | 0,27 | 3,70 |
| <mark>110</mark> | 0,065 | Sand | 1,6 | 160 | 5000 | <mark>20</mark> | 1,37 | 1,09 | 0,27 | 3,70 |
| <mark>120</mark> | 0,080 | Sandy gravel | 1,4 | 140 | 5500 | <mark>15</mark> | 1,52 | 1,09 | 0,36 | 3,06 |
| <mark>130</mark> | 0,085 | Sandy gravel | 1,4 | 140 | 5500 | <mark>15</mark> | 1,47 | 1,12 | 0,38 | 3,06 |
| <mark>140</mark> | 0,090 | Sandy gravel | 1,4 | 140 | 5500 | <mark>15</mark> | 1,43 | 1,15 | 0,36 | 3,06 |
| <mark>150</mark> | 0,095 | Sandy gravel | 1,4 | 140 | 5500 | <mark>15</mark> | 1,39 | 1,19 | 0,38 | 3,06 |



PowerCem technology is available in the UK and enables any materials including organic top soils to be effectively stabilised to build strong, flexible piling mats for both driven and auger piles?

Installing a RoadCem in-situ piling mat will reduce build time by two thirds and provide the piling contractor with a safe flat deflection free mat allowing easy rig set up.

Have you had any of the following problems with a stone piling mat?

- Settlement issues as the weak sub soils compact under the heavy stone mat.
- Mats that need to be far larger than the piling area to allow for the problems of shear.
- Dangers of moving top heavy rigs onto and off the unbound stone mat, at commencement and end of operations.
- Dangers of moving top heavy rigs around the unbound stone mat.
- Unpredictability and delays when setting up the rig for each pile on the unbound stone mat.
- Deflection of the piles due to hard and soft areas/large pieces of stone.
- Heavy rains causing the stone fines to migrate lower in the mat, leaving loose material on top
- Frost getting into trapped water in the mat.
- Piles snagging in the geogrid supporting the stone.
- Costs removing the stone and geogrid/mat is cost consuming and labour intensive.
- All materials used are now classed as contaminated and must be land filled or recycled cleaned). Both costly options.



Benefits of RoadCem soil stabilisation:

- The RoadCem product facilitates a more efficient chemical reaction between the water and cement within the bound material leading to:-
 - Reduction of un-hydrated 'free' cement powder within the mix
 - Reduction of latent water within pores of stabilised materials
 - Can be used to stabilise sulphate bearing soils: Clays, Glacial Tills (Boulder Clays), alluvium soils, sands and Mudstones
 - Greater cement hydration means lower residual pH levels
 - Increased strength characteristics without brittle behaviour
 - Higher flexural stiffness increased Young's Modulus –enhanced flexibility
 - Highly waterproof product no secondary sulphate reaction and no leaching of cement minerals into surrounding soils when saturated for prolonged periods of time

ROBUSTNESS, FLEXURAL STRENGTH, IMPERMEABLE, UNREACTIVE, REVERSIBLE





RoadCem has been used successfully on a number of UK projects to stabilise in-situ soils with high sulphate levels – where the use of standard GGBS has proved insufficient or too expensive to control the reaction.

The high dynamically stiff layer produced by the use of RoadCem means additional engineered benefits can be realised such as thinner bituminous layers as well as a elimination and/or substantial reduction in the thickness of the granular layers.



Independent research published in 2020 has verified the performance of RoadCem in the stabilisation of soils with TPS levels of +10%.



Contents lists available at ScienceDirect

Engineering Science and Technology, an International Journal

journal homepage: www.elsevier.com/locate/jestch

Full Length Article

Incorporation of a nanotechnology-based product in cementitious binders for sustainable mitigation of sulphate-induced heaving of stabilised soils

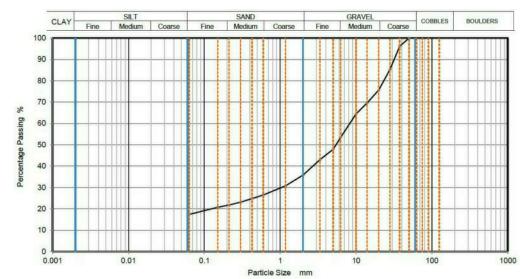
Eyo U. Eyo^{a,*}, Samuel J. Abbey^b, Samson Ngambi^a, Eshmaiel Ganjian^a, E. Coakley^a

^a School of Energy, Construction, Environment, Faculty of Engineering, Environment, Computing, Coventry University, Coventry, United Kingdom ^b Faculty of Environment and Technology, Department of Geography and Environmental Management, Civil Engineering Cluster, University of the West of



Independent laboratory testing carried out in 2020 has also confirmed the performance of RoadCem in the stabilisation of natural soils with TPS levels of +3%. Showing less than 0.1mm soaked swell after 7 days.





| Client: CE Geochem | | Chemtest Job No.: | | | | | |
|-------------------------------------|---------|-------------------|---------|----------|------------------------------|--|--|
| Quotation No.: | (| Chemte | st Sam | ple ID.: | 1075624 Composite SOIL | | |
| | | Clie | ent Sam | ple ID.: | | | |
| | | | Sampl | e Type: | | | |
| | | 01-Oct-2020 | | | | | |
| Determinand | Accred. | SOP | Units | LOD | | | |
| Total Sulphur | U | 2175 | % | 0.010 | 1.0 | | |
| Moisture | N | 2030 | % | 0.020 | 4.6 | | |
| Acid Soluble Sulphur | N | | % | 0.010 | 0.050 | | |
| Water Soluble Sulphur | N | | % | 0.010 | 0.044 | | |
| Oxidisable Sulphides as SO4 | N | | % | 0.030 | 2.9 | | |
| Total Potential Sulphate as SO4 | N | 2175 | % | 0.030 | 3.0 | | |
| pH | U | 2010 | | 4.0 | 9.0 | | |
| Sulphate (2:1 Water Soluble) as SO4 | U | 2120 | g/l | 0.010 | 0.66 | | |
| Sulphate (Acid Soluble) | U | 2430 | % | 0.010 | 0.15 | | |



Independent laboratory testing carried out in 2020 has also confirmed the performance of RoadCem in the stabilisation of natural soils with TPS levels of +3%. Showing less than 0.1mm soaked swell after 7 days.



| Geotech | Califo | rnia Bearing | Job Ref | A200802 Composite | | | |
|---|---|--------------------------|--|--------------------------------------|---|--|--|
| Cutting-Edge Geotechnical | Camo | inia bearing | Borehole/Pit No. | | | | |
| Site Name | Wilton International | Port | Sample No. | Roadcem/CEM1 | | | |
| Soil Description | Grey mudstone | | | | Depth m | 0.00 | |
| Specimen Curing Time | 4 day | 4 day Target Moisture | | % % | Sample Type | AMAL | |
| Specimen Description | Specimen 5 (Swell) | - Top of mould | | | KeyLAB ID | CEGL202010013 | |
| Test Method | BS EN 13286 - Par | 47 : 2004 | | | Date of Test | 19/10/2020 | |
| | REMOULDED Recompacted rammer etained on 20mm siev bother details Bu Do | I with specified stan | dard effort using 24 2.32 2.13 8.9 | 4.5kg % Mg/m ³ % | Soaking details Period of soaking Time to surface Amount of swell recorded Dry density after soaking Surcharge applied | 7 days N/A days 0.09 mm 2.13 Mg/m ³ 0 kg 0 kPa | |
| 50.00 45.00 40.00 35.00 25.00 25.00 20.00 15.00 10.00 | | | | | | —— Data = 2.5 mm == 5.0 mm Correction | |
| 5.00 0.00 0 Results | 1 2 Curve correcti applie | on CBR V | 4 5 ration mm 'alues, % mm Highest | | 7 8 Moisture Content % | | |

Traditional aggregate and Geogrid solution vs RoadCem method

TOPSOIL LAYER



Because the RoadCem layer will be around ten times stiffer than the stone layer, even allowing for the Geogrid support, the engineered thickness can be as much as a third the thickness.

When produced from the existing site soils replacement of soils with imported stone is never needed.

IN-SITU SUBSOIL

RoadCem Stabilised Layer

The stone piling mat will suffer from weather/water damage and will need continued maintenance.

IN-SITU SUBSOIL

SUBSOIL REMOVED AS WASTE OR STOCKPILED

TOPSOIL LAYER

IMPORTED AGGREGATE

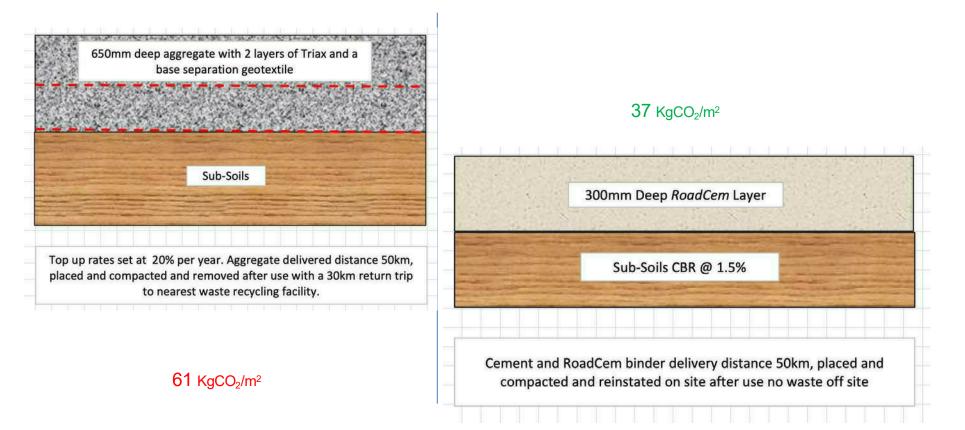
GEOGRID REINFORCEMEN

The RoadCem piling mat has a frost and water resistant surface and will need no maintenance



RoadCem – Sustainability Comparisons

Traditional aggregate haul road compared to a RoadCem single layer solution



PGG S

RoadCem – Environmental benefits



REDUCE Vehicle Movements

Eliminate the need for aggregate imports to site and the export disposal of any surface layers after use.

+85% Typical Reduction Achievable

MINIMISE CO₂ – Use the most sustainable solution

LCA assessments show that by adopting a single layer solution embedded CO₂ can be kept to an absolute minimum

>20% CO₂ reduction over soil enhancement >60% CO₂ reduction over aggregate solutions

SAVE TIME – Reduce Construction Programmes

A RoadCem solution can save weeks of programme time with +2000m² of single layer product installed each day

Up to 90% reduction in programme time



RoadCem – Working Platforms

Designed using the new TWF Design Methodology





Working Platforms Design of granular working platforms for construction plant A guide to good practice



Published by Temporary Works Forum, do Institution of CMI Engineers, One Great George Street, London, SWIP 3AA, England

First Published: April 2019

This TWF Guidance is available as a free download from www.twforum.org.uk

Document: TWf2019: 02

NOTE: If you need to print this document, be aware that the pages are prepared with attends (even) pages offset for your duplex (double sided) printing.





Research set-up into the Visco-Elastic Behaviour of RoadCem Piling Mats

In tests carried out by Delft University a single size sand (1780/m3) was used (fractions 0.5/1mm) in addition to 0.09% m/m of RoadCem material in relation to sand, as well as 9.14% m/m OPC (CEM 1 42.5 N).

The OMC (optimum moisture content) at MPD (maximum proctor density) was 11% m/m.

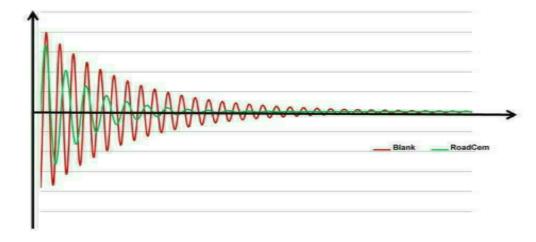
The reference mixture was composed with 9,14 m/m OPC (CEM 1 42.5N) under equal conditions prepared without any RoadCem added. The visco-elastic and ductility properties of RoadCem were found by conducting dynamic tests.

Dynamic Testing

These dynamic tests are carried out using non-destructive ultra-waves in order to determine the dynamic- elastic modulus. By means of destructive four- point bending tests in which repetitive loads at a fixed frequency are applied, a superior fatigue performance is confirmed.

By observing the longitudinal displacement mode after excitation, the dynamic modulus is obtained, as well as the dampening characteristics, which relate to the visco-elastic properties of the material being tested.

It is very clear that the pattern for cement treated stabilisation with added RoadCem (shown green) is showing a restrained vibration compared to the cement alone stabilised material (shown as red) this will improve safety during piling, reducing BOUNCE and improving alignment.



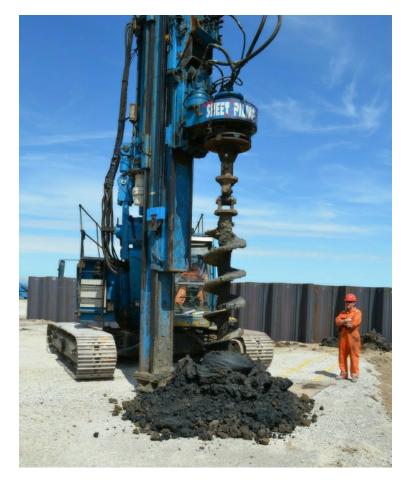


Delft University of Technology



All types of piling rigs and cranes can be used safely & effectively on a RoadCem piling mats











- Existing very soft made ground at Hull WWTW
- Mott MacDonald Bentley project
- Soft ground stabilised to enable site piling and lifting operations to be safely carried out.

- RoadCem working platform ready for use.
- Allowing piling rig and crawler crane to operate directly on the RoadCem layer. No surface stone layer required.









- During even the wettest conditions RoadCem platform allows heavy construction work to meet challenging programmes.
- Piling, Crane lifts, MEWP, laydown all perfectly supported straight off the RoadCem surface.







Walton on Thames Road Bridge for Costain / Atkins

RoadCem soil stabilisation is up to 12x stiffer than stone for piling mats and heavy crane/rig platforms.

Soil stabilisation is a sustainable method for the construction of insitu bound soil base for infrastructure applications.

Where longer lasting and/or heavier loadings are required RoadCem is the proven answer. Just a 1% addition by weight of cement enables cement to become a far superior soil binder.

Winner of multiple industry awards the Walton on Thames Road bridge built for Surrey County Council by Costain/Atkins used cement with added RoadCem to create really strong bound soil crane and piling rig platforms from the existing alluvial site soils.

With no added surface protection and/or cover these stabilised soil working platforms were used for the two-year construction period without damage by heavy plant and crawler cranes.



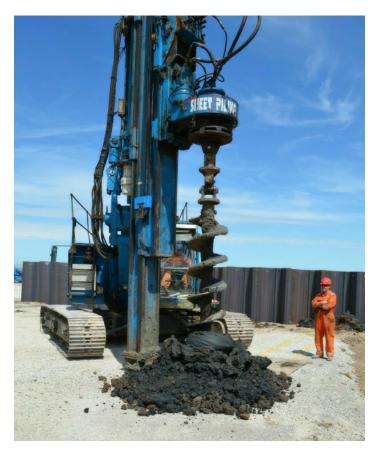
Walton on Thames Bridge Project of the Year Winner £10-£50 million



CIVIL ENGINEERING



- RoadCem working platform for construction of new terminal surface water pumping station on the Sandringham Estate at Wolferton
- Heavy plant working over soft silty soils with high water table
- Platform rotovated back to granulised soil and returned to nature upon completion within arable land areas.



- Note: soft organic silty soil underlying platform
- Sheet piling driven through RoadCem platform without any localized overbreak











- Office headquarters project
- RoadCem piling mat and working platform
- RoadCem stabilised layer replaced all permanent road subbase stone
- RoadCem layer under external block paved areas forming new car parks



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